A Flexible Frequency and Pattern Reconfigurable Antenna for Wireless Systems

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Abstract—A novel flexible frequency and pattern reconfigurable antenna for wireless system is proposed. The antenna is composed of two completely symmetrical radiating elements, a feedline and ground. By controlling the on and off of 8 PIN diodes loaded on the symmetric hexagonal split ring and monopole branches to select the radiation element, the antenna achieves frequency reconfiguration in 1.9G band and 2.4G band, and is capable of steering the beam in two directions in each band. Meanwhile, the antenna works at four states with omnidirectional radiation patterns. Finally, the bending characteristics of the antenna at different bending degrees are analyzed. Measured results are in good agreement with simulations, which denotes that it is suitable for wireless systems.

1. INTRODUCTION

With successive development of wireless systems, flexible reconfigurable antennas have attracted much attention due to the features of flexibility and reconfigurability. Flexible material and reconfigurable antenna are combined to form a flexible reconfigurable antenna, which not only has the advantages of flexibility, good fit for the carrier, effective space saving, and small system volume, but also can use an antenna to achieve the function of multiple single antennas. Therefore, the research of flexible reconfigurable antennas has significance in today's complex environment. In [1], a frequency and pattern reconfigurable antenna based on a center-shorted microstrip patch is presented. The antenna can switch its operation between two distinct configurations, namely a microstrip patch broadside pattern or an omnidirectional monopole pattern by utilizing varactors loaded with open-circuited stubs as its tuning mechanism. A novel patch antenna with frequency and pattern reconfiguration with polarization switching is proposed, which could select the rhombus-shaped radiator with three excitation lines oriented at different angles by changing the bias states of three pairs of PIN diodes [2]. A flexible reconfigurable folded slot antenna based on a flexible polyethylene terephthalate substrate is presented. The frequency and polarization reconfigurability is achieved by turning a PIN diode on and off, which alters the radiation characteristics of the stub [3]. In [4], an optically transparent, flexible, and mechanically reconfigurable zeroth-order resonant antenna using a stretchable micromesh structure is presented, and the resonant frequency of the antennas is linearly reconfigurable from 2.94 to 2.46 GHz upon stretching. A diode-switched thermal-transfer printed antenna on a flexible substrate achieves frequency reconfigurability [5]. A robust, flexible, and electronically tunable wearable antenna is designed and fabricated on a PDMS substrate, and conductive fabric is used to form the conducting parts of the antenna. The frequency-reconfigurability is achieved by means of varactors [6].

In this paper, a frequency and pattern reconfigurable antenna based on flexible materials for wireless application is proposed. By controlling PIN diodes, the proposed antenna achieves frequency

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reconfiguration in 1.9G band and 2.4G band. When operating at 1.9G band, the antenna can switch the pattern in the direction of $\phi = 60^{\circ}$ and $\phi = 300^{\circ}$. When operating at the 2.4G band, the antenna can switch the pattern in the direction of $\phi = 34^{\circ}$ and $\phi = 326^{\circ}$. The proposed antenna with bias lines is fabricated on a Rogers 5880 substrate.

2. ANTENNA DESIGN

The frequency and pattern reconfigurable antennas are able to control the resonant frequency band and radiation direction by selecting the radiator through PIN diodes, MEMS, or varactors, which are used to dynamically change the antenna radiation performance. The dielectric substrates used for flexible antennas are textile, paper-based, polymer (polyimide, PDMS, PET, LCP, etc.), Rogers flexible substrate.

The geometry and design parameters of the proposed flexible frequency and pattern reconfigurable antenna are shown in Fig. 1. The antenna is composed of a feedline, a ground and two completely symmetrical radiating elements, wherein each radiating element comprises a circular monopole branch, a regular hexagonal open ring, and two branches are added to the ring to extend the current and lower the low frequency to get the desired frequency band, which are fabricated on a Rogers5880 substrate with a relative permittivity of 2.2 and thickness of 0.127 mm. To select the radiated element, we can control the on and off of 8 PIN diodes loaded on the symmetric radiation element. The parameters are optimized by the commercial software ANSYS high frequency structure simulator (HFSS) v15.0. The dimensions of the flexible frequency and pattern reconfigurable antenna are: L = 44 mm, W = 42 mm, L1 = 12 mm, W1 = 1.5 mm, L2 = 10 mm, W2 = 2 mm, L3 = 11 mm, L4 = 7 mm, W3 = 0.8 mm, W4 = 4 mm, W5 = 4 mm, L5 = 10 mm.

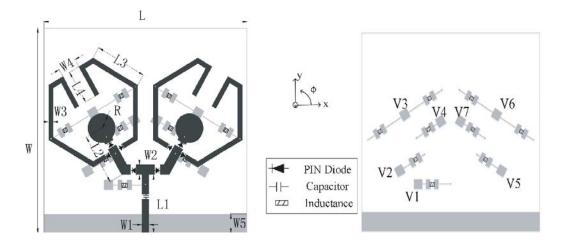


Figure 1. Geometry of the flexible reconfigurable antenna.

Because the diode requires a DC bias voltage to control its ON or OFF state, bias voltages of V1 to V7 are applied. The PIN diode is SMP1345 series, and the operating frequency range is 100 MHz to 6 GHz. From the characteristic parameters of the SMP1345_079 series, the equivalent resistance of the PIN diode for the ON state is 1.5Ω , whereas the equivalent capacitance for the OFF state is 0.19 pF. Bias voltage and the states of PIN diodes in the two modes of the antenna are displayed in Table 1. Moreover, a 470 pF Murata is mounted on the feedline to avoid DC signal flowing into the RF source of the antenna, and the maximum operating frequency of this capacitor is 8.5 GHz. In order to isolate the DC and RF signals, each bias contains an RF choke inductor L of 100 nH.

The current distributions in the four operating states are illustrated in Fig. 2. At different states, the radiation patch is altered and current distribution changed, which eventually switches the antenna's radiation direction. The activated radiator has strong current density, whereas the disconnected radiator has low current density on its surface.

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states	V1	V2	V3	V4	V5	V6	V7	P1	P2	P3	P4	P5	P6	P7	P8
S1	2V	1V	0V	/	/	/	/	ON	ON	ON	OFF	OFF	OFF	OFF	OFF
S2	2V	1V	/	0V	/	/	/	ON	OFF	OFF	ON	OFF	OFF	OFF	OFF
S3	2V	/	/	/	1V	0V	/	OFF	OFF	OFF	OFF	ON	ON	ON	OFF
S4	2V	/	/	/	1V	/	0V	OFF	OFF	OFF	OFF	ON	OFF	OFF	ON

Table 1. Four modes of the proposed flexible reconfigurable antenna.

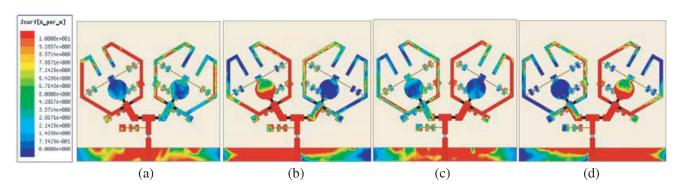


Figure 2. The current distribution in the four operating states. (a) S1. (b) S2. (c) S3. (d) S4.

3. RESULTS AND DISCUSSION

The flexible pattern reconfigurable antenna is fabricated, shown in Fig. 3. PIN diodes of SMP1345 are soldered, which are assured by low capacitance and low resistance. The S-parameters of the proposed reconfigurable antenna are measured by the Agilent E8363B vector network analyzer. By controlling PIN diodes, the proposed antenna achieves frequency reconfiguration in the 1.9G band with a bandwidth of 1.84–2.00 GHz and the 2.4G band with a bandwidth of 2.27–2.49 GHz. When operating at the 1.9G band, the antenna can switch the pattern in the direction of $\phi = 60^{\circ}$ and $\phi = 300^{\circ}$. When operating at 2.4G band, the antenna can switch the pattern in the direction of $\phi = 34^{\circ}$ and $\phi = 326^{\circ}$. The measured and simulated input reflection coefficients at different states are shown in Fig. 4. Simulated and measured radiation patterns at different states are shown in Fig. 5 and Fig. 6. The simulation and measurement of the two states are basically in agreement. Through the comparison and analysis

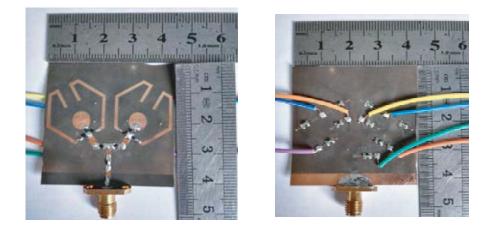


Figure 3. Photograph of the fabricated reconfigurable antenna.

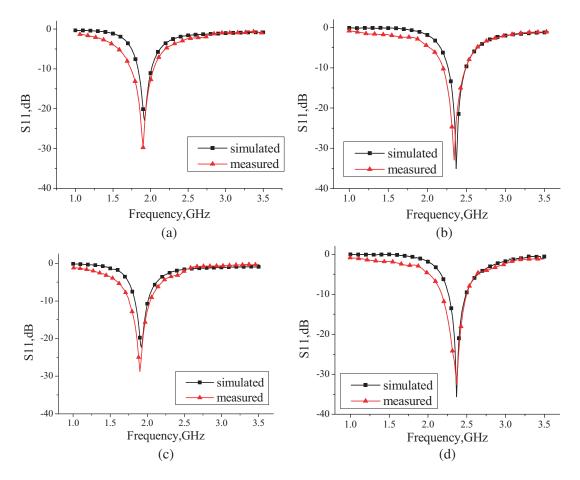


Figure 4. The measured and simulated reflection coefficients for four different states of the flexible frequency and pattern reconfigurable antenna. (a) S1. (b) S2. (c) S3. (d) S4.

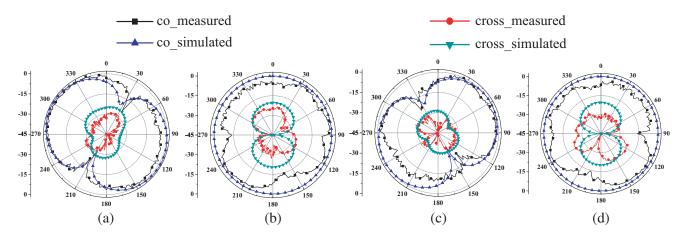


Figure 5. Radiation-patterns for different states of the proposed antenna at 1.9 GHz. (a) E plane at S1. (b) H plane at S1. (c) E plane at S3. (d) H plane at S3.

of the simulated and measured results, we can see that the measured bandwidth is slightly wider than the simulation one. The E-planes of radiation-patterns show an "8" shape, and the H-planes show omni-direction, which are in accordance with simulated results. However, there are some bump places in the measurement which are inconsistent with the simulation in the radiation-patterns. Those are

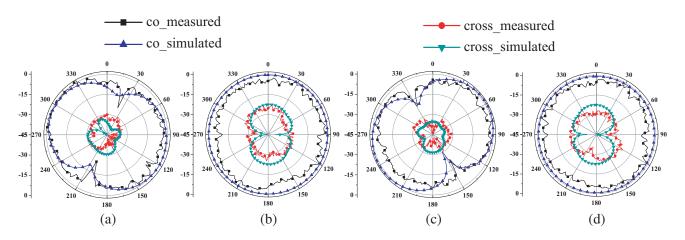


Figure 6. Radiation-patterns for different states of the proposed antenna at 2.4 GHz. (a) E plane at S2. (b) H plane at S2. (c) E plane at S4. (d) H plane at S4.

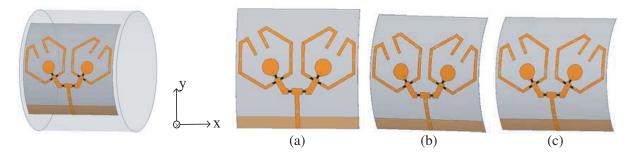
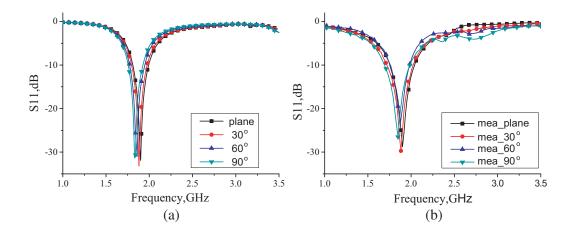


Figure 7. The simulation model corresponding to different bending angles. (a) 30° . (b) 60° . (c) 90° .

due to the device error in frequency response, because the model parameters of the PIN diodes used in the simulation usually have a certain drift with the frequency. In addition, the external DC bias line, welding errors and testing environment have a certain impact on antenna radiation.

Then, the influence of different bending degrees on the antenna is analyzed. Since the width along the x-axis is narrow and the SMA is welded, it is not easy to bend along the x-axis. The proposed flexible frequency and pattern reconfigurable antenna is bent in the y-axis direction, and Fig. 7 shows the simulation model corresponding to different bending angles. Due to the symmetrical structure of the antenna, only states S3 and S4 are studied here. The measured and simulated input reflection



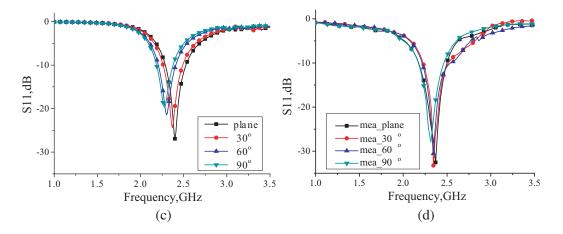


Figure 8. The reflection coefficients at different bending levels along y-axis. (a) Simulated result of S3. (b) Measured result of S3. (c) Simulated result of S4. (d) Measured result of S4.

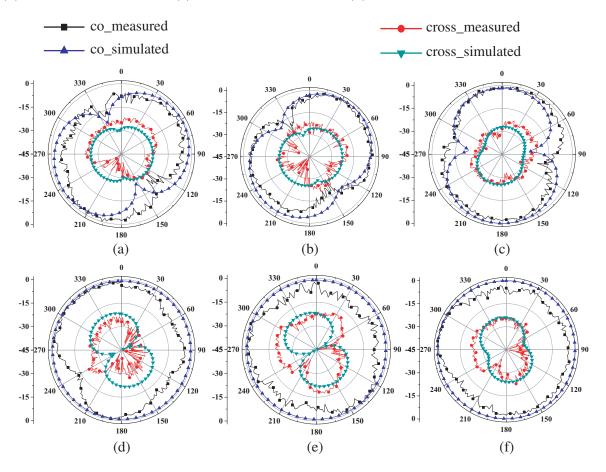


Figure 9. The radiation-pattern of S3 at different bending levels along y-axis. (a) E plane at 30°. (b) E plane at 60°. (c) E plane at 90°. (d) H plane at 30°. (e) H plane at 60°. (f) H plane at 90°.

coefficients at different bending levels are shown in Fig. 8. Simulated and measured far-field radiation patterns at different bending levels for the two different states are shown in Fig. 9 and Fig. 10.

From the result of reflection coefficients, it is observed that the resonant frequency of 1.9G band moves to low frequency as the bending degree increases, but $|S_{11}| \leq -10$ dB does not deteriorate, and the frequency characteristics of the antenna basically meet the design requirements, and that the resonant

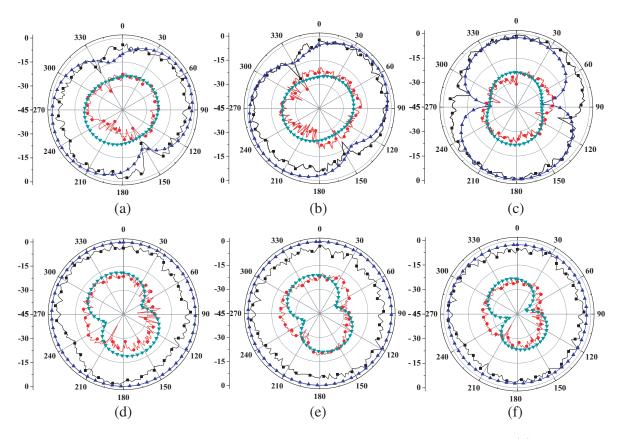


Figure 10. The radiation-pattern of S4 at different bending levels along y-axis. (a) E plane at 30° . (b) E plane at 60° . (c) E plane at 90° . (d) H plane at 30° . (e) H plane at 60° . (f) H plane at 90° .

frequency of 2.4G band moves to low frequency as the bending degree increases, and $|S_{11}| \leq -10 \,\text{dB}$ is not significantly deteriorated, but the bandwidth of the antenna gradually deviates from the design requirements. Because with the antenna bending, the length of the patch is extended, the current path is lengthened and frequency decreased. With the increase of bending degree, the change of S4 state is smaller than that of S3 state, because S4 state is radiated by circular patch, and its position is close to the symmetry axis, so the relative position of the radiation patch changes slightly when the antenna is bent. By comparing the patterns, the radiation direction of the pattern gradually increases toward 0° in the clockwise direction, and the cross polarization increases as the degree of bending increases. The measured results are consistent with the simulated ones.

4. CONCLUSION

A novel flexible frequency and pattern reconfigurable antenna for wireless system is proposed. The antenna consists of two completely symmetrical radiating elements, a feedline and ground. 8 PIN diodes are loaded on the symmetric hexagonal split ring and monopole branches to select the radiation element. By controlling PIN diodes, the proposed antenna achieves frequency reconfiguration in the 1.9G band with a bandwidth of 1.84–2.00 GHz and the 2.4G band with a bandwidth of 2.27–2.49 GHz, and it is capable of steering the beam in two directions in each band. Meanwhile, the antenna works at four states with omnidirectional radiation patterns. Finally, the bending characteristics of the antenna at different bending degrees is analyzed, and we find that within a certain bending range, the antenna can still meet the requirements. Measured results are in good agreement with simulations, which denotes that it is suitable for wireless systems.

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