## A NEW ACCURATE VOLTERRA-BASED MODEL FOR BEHAVIORAL MODELING AND DIGITAL PREDISTOR-TION OF RF POWER AMPLIFIERS

# T. Du<sup>\*</sup>, C. Yu, Y. Liu, J. Gao, S. Li, and Y. Wu

School of Electronic Engineering, Beijing University of Posts and Telecommunications, P. O. Box 171, Beijing, China

Abstract—A new accurate Volterra-based model is introduced for behavioral modeling and digital predistortion (DPD) of power amplifiers (PAs). This model extends the GMP model with specific cross terms, and these augmented terms significantly increase the model's performance. The proposed model's performance is assessed using a LDMOS Doherty PA driven by two modulated signals (a 4-carrier WCDMA signal and a single carrier 16QAM signal). The experimental results in both behavioral modeling and DPD applications demonstrate that the proposed model outperforms the hybrid memory polynomial-envelope memory polynomial (HME) model and generalized memory polynomial (GMP) model. Compared with the HME model, the proposed model shows an average normalized mean square error (NMSE) improvement of 2.2 dB in the behavioral modeling, average adjacent channel power ratio (ACPR) improvement of 2.8/2.5 dB in the DPD application, and 20% reduction in the number of coefficients. In comparison with the GMP model, the proposed model achieves higher model accuracy and better DPD performance, but reduces approximately 40% of coefficients.

## 1. INTRODUCTION

Radio frequency (RF) power amplifiers (PAs) are one of the most important components in wireless communication systems, but they are also the major source of nonlinearity. Many linearizing techniques are used in the power amplifiers [1–3]. Compared with the analog linearizing methods, processing the base band signals in the digital area

Received 27 March 2012, Accepted 9 May 2012, Scheduled 23 May 2012

<sup>\*</sup> Corresponding author: Tianjiao Du (dutianjiao@bupt.edu.cn).

has many advantages such as high flexibility, applicability, and easy to realize the adaptive processing. Therefore, it has great potential to research and develop the digital predistortion (DPD) technique [1].

One of the main challenges in developing effective DPD technique is to find a way to capture the nonlinear distortion and memory effects of the PA using an accurate behavioral model. Volterra series can accurately describe the nonlinear system, but it involves a great number of coefficients [4–8]. Several behavioral models have been proposed for PAs and transmitters, such as the Memory Polynomial (MP) model, Envelope Memory Polynomial (EMP) model, HME model, and GMP model [9–13]. The MP model contains the diagonal terms of Volterra series, while the EMP model is composed of cross items between the signal and lagging exponentiated envelope terms, and the two models combine together to form the HME model. It has been confirmed that the HME model outperforms the MP model and EMP model. The GMP model combines the MP model with cross terms between the signal and lagging and/or leading exponentiated envelope terms. It can be seen that the cross terms introduced by the EMP model are special cases of the GMP model's lagging cross terms. Though several behavioral models have been proposed and applied to DPD, the study on modeling technique is still far from being mature since accurately characterizing RF PAs becomes more and more difficult as wireless communication systems migrate to higher frequencies, higher speeds, and wider bandwidths.

In this paper, we present a new accurate Volterra-based behavioral model for behavioral modeling and DPD of RF PAs. In fact, the proposed model can be applied to nonlinearity compensation in a variety of dynamic nonlinear systems used in industrial electronic Since this model has linear dependence on the applications. coefficients, the estimation of these coefficients can be achieved by any least-squares (LS) type of algorithm [13]. In addition, the number of coefficients can be controlled through a proper choice of model dimensions. The model's performance in behavioral modeling and DPD applications is assessed using a LDMOS Doherty PA, and two test signals (a 4-carrier WCDMA signal and a single carrier 16QAM signal) are used for verifications. This paper also presents a thorough comparison between the proposed model and the HME model, as well as the GMP model. Normalized mean square error (NMSE) and error power spectral density (EPSD) are considered to evaluate the model accuracy while adjacent channel power ratio (ACPR) is used to assess the DPD application [14-17]. The computational complexity is characterized by the number of coefficients required for each model [17]. The comparison results fully illustrate that the new model outperforms

the other two models with the least number of coefficients in both behavioral modeling and DPD applications.

## 2. VOLTERRA-BASED BEHAVIORAL MODELS

The MP model takes the diagonal terms of Volterra series, and its mathematical formulation is given by [9, 10]

$$y_{\rm MP}(n) = \sum_{k=1}^{K} \sum_{q=0}^{Q} a_{kq} x(n-q) \left| x(n-q) \right|^{k-1}$$
(1)

where x(n) and  $y_{\text{MP}}(n)$  are the input and output waveforms of the MP model, respectively. Q, K and  $a_{kq}$  are the memory depth, nonlinearity order, and model coefficients, respectively.

When the complex gain of the PA is only a function of the magnitude of the input signal, EMP can be used, and the corresponding formulation is [11]

$$y_{\rm EMP}(n) = \sum_{k=1}^{K} \sum_{q=0}^{Q} a_{kq} x(n) \left| x(n-q) \right|^{k-1}$$
(2)

where x(n) and  $y_{\text{EMP}}(n)$  are the EMP model input and output waveforms, respectively. Q, K and  $a_{kq}$  are the memory depth, the nonlinearity order, and the model coefficients, respectively. Compared with the MP model, the EMP model has an easier structure.

To combine the benefits of the two models mentioned above, the HME model is proposed in [12]. It is demonstrated that the HME model achieves better modeling accuracy than each sub-model. The analytical formulation of the HME model is given by

$$y_{\text{HME}}(n) = \sum_{k=1}^{K_a} \sum_{q=0}^{Q_a} a_{kq} x(n-q) |x(n-q)|^{k-1} + \sum_{k=1}^{K_b} \sum_{q=0}^{Q_b} b_{kq} x(n) |x(n-q)|^{k-1}$$
(3)

where x(n) and  $y_{\text{HME}}(n)$  are the input and output waveforms of the HME model, respectively.  $K_a$ ,  $Q_a$  and  $a_{kq}$  are the nonlinearity order, memory depth, and model coefficients of the MP sub-model, respectively. Equivalently,  $K_b$ ,  $Q_b$  and  $b_{kq}$  are the nonlinearity order, memory depth, and model coefficients of the EMP sub-model, respectively. In the GMP model [13], the estimated output waveform is related to the input waveform by

$$y_{\text{GMP}}(n) = \sum_{k=1}^{K_a} \sum_{q=0}^{Q_a} a_{kq} x(n-q) |x(n-q)|^{k-1} + \sum_{k=2}^{K_b} \sum_{q=0}^{Q_b} \sum_{l=1}^{L_b} b_{kql} x(n-q) |x(n-q-l)|^{k-1} + \sum_{k=2}^{K_c} \sum_{q=0}^{Q_c} \sum_{l=1}^{L_c} c_{kql} x(n-q) |x(n-q+l)|^{k-1}$$
(4)

where x(n) and  $y_{\text{GMP}}(n)$  are the input and estimated output waveforms of the GMP model, respectively.  $K_a$ ,  $Q_a$  and  $a_{kq}$  are the nonlinearity order, memory depth, and coefficients of the aligned terms between signal and its exponentiated envelope, respectively.  $K_b$ ,  $Q_b$ ,  $L_b$  and  $b_{kql}$ are the nonlinearity order, memory depth, lagging cross terms index, and coefficients of the signal and lagging exponentiated envelope terms, respectively.  $K_c$ ,  $Q_c$ ,  $L_c$  and  $c_{kql}$  are the nonlinearity order, memory depth, leading cross terms index, and coefficients of the signal and leading exponentiated envelope terms, respectively.

Actually, for the behavioral models mentioned above, it is reasonable to consider only odd-order nonlinearities because the effects from even order kernels can be omitted in a band-limited modulation system [5].

# 3. DISCRIPTION OF THE NEW VOLTERRA-BASED MODEL

Discrete-time finite-memory complex baseband Volterra series can be used to describe a nonlinear PA of a wireless communication system, the mathematical formulation is given by [8]

$$y(n) = \sum_{\substack{k=1\\k-odd}}^{K} \sum_{q_k=0}^{Q_k} h_k(q_k) x(n-q_1) \prod_{m=1}^{(k-1)/2} x(n-q_{2m}) x^*(n-q_{2m+1})$$
(5)

where the first summation is restricted to odd values of k; x(n) and y(n) represent the input and output complex envelope samples of PA;  $h_k(q_k)$  represents the discrete-time Volterra kernels of order k;  $q_k$  is composed of the integer-valued delays,  $q_k = 0, \ldots, Q_k$  for all  $k = 1, 3, \ldots, K$ . Here we consider decaying memory with the same finite length  $Q_k = Q$  for all order k.

#### Progress In Electromagnetics Research C, Vol. 29, 2012

The Volterra series model provides a general way to describe the nonlinear system, but the number of coefficients to be estimated increases exponentially with the degree of nonlinearity and memory depth of the system. The complexity of the Volterra series model is revealed in the fact that the kernels  $h_k(q_k)$  form an k-dimensional grid defined by the discrete delays in each axis of the multidimensional space  $q_1, q_2, \ldots, q_k$ . Therefore, it is desirable to reduce the number of these delays [7].

Firstly, consider the case that input samples are all at the same time instant, i.e.,  $q_1 = q_2 = \ldots = q_k = q$ , thereby generating a twodimension (2-D) array from (5). Actually, this is the so-called MP model and it can be written as

$$y_{2-D}(n) = \sum_{\substack{k=1\\k-odd}}^{K} \sum_{q=0}^{Q} h_{kq} x(n-q) \left| x(n-q) \right|^{k-1}$$
(6)

Then relax the restriction condition and consider another case that just one time delay distinguishes itself from the others. Assuming that the special time delay is q, the corresponding signal is a x term, while the others are all equal to q - l ( $l \ge 1$ ). Then the first 3-D array is generated from (5) and it can be expressed as

$$y_{3-D,1}(n) = \sum_{\substack{k=1\\k-odd}}^{K} \sum_{q=0}^{Q} \sum_{l=1}^{L} h_{kql}^{(1)} x(n-q) \left| x(n-q-l) \right|^{k-1}$$
(7)

When q = 0, it can be seen that (7) degenerates into an EMP model, as described in (2). Furthermore, the degraded (7) and (6) constitute the HME model.

If the other time delays are all equal to q + l  $(l \ge 1)$ , we can formulate the second 3-D array as

$$y_{3-D,2}(n) = \sum_{\substack{k=1\\k-odd}}^{K} \sum_{q=0}^{Q} \sum_{l=1}^{L} h_{kql}^{(2)} x(n-q) \left| x(n-q+l) \right|^{k-1}$$
(8)

It can be seen that Equation (6) together with (7) and (8) lead to the GMP model. Similarly, if the signal with the special time delay is a  $x^*$  term, another two 3-D arrays are achieved

$$y_{3-D,3}(n) = \sum_{\substack{k=3\\k-odd}}^{K} \sum_{q=0}^{Q} \sum_{l=1}^{L} h_{kql}^{(3)} x^* (n-q) x^2 (n-q-l) \left| x(n-q-l) \right|^{k-3}$$
(9)

and

$$y_{3-D,4}(n) = \sum_{\substack{k=3\\k-odd}}^{K} \sum_{q=0}^{Q} \sum_{l=1}^{L} h_{kql}^{(4)} x^* (n-q) x^2 (n-q+l) \left| x(n-q+l) \right|^{k-3}$$
(10)

It is obvious that if we continue this process, more items will be produced, which is not feasible for practical application. Thus we put a termination to the process, the resulting outputs  $y_{2-D}(n)$ ,  $y_{3-D,1}(n)$ ,  $y_{3-D,2}(n)$ ,  $y_{3-D,3}(n)$  and  $y_{3-D,4}(n)$  are additively combined to construct the overall output signal of the new Volterra-based model, and its analytical formulation is given by

$$y(n) = y_{2-D}(n) + \sum_{m=1}^{4} y_{3-D,m}(n)$$
(11)

where y(n) is the output waveforms of the new pruned Volterra series model.

In most real PAs, the static nonlinearities and low-order dynamics are the dominant sources of the distortions induced by the PA [12]. In addition, the GMP model (Equation (6) together with (7), (8)) has proven effective for predistortion of actual PAs [13,17]. Equations (9) and (10) can be seen as supplements to the GMP model, so it is reasonable to just retain the 3rd-order dynamics of Equations (9) and (10) to reduce the model complexity. Furthermore, there is no need to take the same model dimensions for all the arrays. They can be controlled separately, which leads to a reasonable total number of coefficients while maintaining acceptable performance. Finally, Equation (11) is further simplified as follows

$$y(n) = \sum_{\substack{k=1\\k-odd}}^{K_a} \sum_{q=0}^{Q_a} a_{kq} x(n-q) |x(n-q)|^{k-1} + \sum_{\substack{k=3\\k-odd}}^{K_b} \sum_{q=0}^{Q_b} \sum_{l=1}^{L_b} b_{kql} x(n-q) |x(n-q-l)|^{k-1} + \sum_{\substack{k=3\\k-odd}}^{K_c} \sum_{q=0}^{Q_c} \sum_{l=1}^{L_c} c_{kql} x(n-q) |x(n-q+l)|^{k-1} + \sum_{\substack{q=0\\q=0}}^{Q_d} \sum_{l=1}^{L_d} d_{ql} x^* (n-q) x^2 (n-q-l)$$

 $\mathbf{210}$ 

Progress In Electromagnetics Research C, Vol. 29, 2012

$$+\sum_{q=0}^{Q_e}\sum_{l=1}^{L_e} e_{ql} x^* (n-q) x^2 (n-q+l)$$
(12)

where  $K_a$ ,  $K_b$  and  $K_c$  are the nonlinearity order of the first three arrays, respectively.  $Q_a$ ,  $Q_b$ ,  $Q_c$ ,  $Q_d$  and  $Q_e$  are the memory depth of the five arrays, respectively.  $L_b$ ,  $L_c$ ,  $L_d$  and  $L_e$  are the corresponding lagging or leading cross terms index of the last four arrays, respectively.  $a_{kq}$ ,  $b_{kql}$ ,  $c_{kql}$ ,  $d_{ql}$  and  $e_{ql}$  are the coefficients of the proposed model. Like those of the GMP model, the coefficients can be simply and robustly estimated using any least-squares type of algorithm. This has favorable implications for algorithm stability and computational complexity [13].

Apparently, the new Volterra-based model extends the GMP model with specific cross terms. Compared with the GMP model, the proposed model dimensions are defined by four more variables, but the augmented terms further increase the accuracy of the model. In addition, the model's complexity can be controlled through the proper choice of the model dimensions.

### 4. THE EXPERIMENTAL RESULTS AND DISCUSSION

In order to validate the proposed behavioral modeling technique in a real system, a highly nonlinear 80 W LDMOS Doherty PA ( $V_{ds} = 28 \text{ V}$ ,  $V_{gs} = 5.6 \text{ V}$ ) was tested. This PA was operated at 1.96 GHz and excited by a 4-carrier WCDMA signal (PAPR = 8.7 dB) and a 15 MHz data ratesingle carrier 16QAM signal (PAPR = 6.2 dB). Fig. 1 shows the test bench set-up.



Figure 1. Experiment test bench.

This experimental setup was composed of a LDMOS Doherty PA, a vector signal generator (N5182A), a vector signal analyzer (VSA), and a computer. The computer was used to download signals into the N5182A that drove the PA with the RF input signals. The output signals of the PA was attenuated and then down-converted and demodulated within the VSA. MATLAB software was then applied to behavioral modeling and DPD. 4000 samples of the input and output waveforms were used for model identification employing the LS (Least Squares) algorithm [17]. For comparison, we also implemented the HME model, the GMP model and they are represented as Model M1 and Model M2 respectively in the following measure results. The proposed model as shown in (12) is called Model M3.

### 4.1. Model Accuracy Evaluation

For each test signal, the HME model, GMP model, and the proposed model were all identified. Two assessments were considered to evaluate the model accuracy: NMSE in the time domain and EPSD in the frequency domain [14–17].

The MP sub-model dimensions are estimated using a general sweep method [17]. The memory depth is swept from 0 to 5, and the nonlinearity order is swept from 1 to 13. Fig. 2 shows the NMSE values versus the memory depth  $K_a$  and nonlinearity order  $Q_a$  obtained for the 4-carrier WCDMA signal. Accordingly, the dimensions of the MP sub-model are set to  $K_a = 9$  and  $Q_a = 3$ .



Figure 2. NMSE values versus the nonlinearity order and memory depth of the MP sub-model.

#### Progress In Electromagnetics Research C, Vol. 29, 2012

For the sake of reducing model complexity, the lagging or leading cross terms indexes  $(L_b, L_c, L_d \text{ and } L_e)$  and the memory depths of the added cross terms  $(Q_d \text{ and } Q_e)$  are set to 1. In order to avoid accidental results,  $K_b/K_c$  and  $Q_b/Q_c$  are set to different values and the corresponding NMSEs are summarized in Table 1.

As highlighted in Table 1, compared with the HME model, the proposed model shows a NMSE improvement of  $1.6 \,\mathrm{dB}$  with 80% coefficients. The GMP model performance in terms of NMSE does not exceed  $-37 \,\mathrm{dB}$  even if the number of parameters is increased far above the total number of parameters that are used for the proposed model to achieve an NMSE that exceeds  $-37.18 \,\mathrm{dB}$ . In this case, the EPSD plots along with the original PA output spectra are shown in Fig. 3. This figure makes it clear that the proposed model also achieves the best performance in the frequency domain.

These models were also identified for the single carrier 16QAM signal, model dimensions were set to different values as used for the 4-carrier WCDMA signal. Fig. 4 shows the comparison of the three models in terms of the NMSE as a function of the number of coefficients. This figure clearly illustrates the advantage of the proposed model in terms of the NMSE. In the case that stressed in Fig. 4, the EPSD plots along with the original PA output spectra are shown in Fig. 5. Obviously, the proposed model achieves the lowest error in the frequency domain.

According to the calculated results in terms of NMSE, EPSD



Figure 3. EPSD plots for the 4-carrier WCDMA signals test.



Figure 4. Comparison of the three models in terms of the NMSE as a function of the number of coefficients. Each point is represented by the lower NMSE at each number of coefficients.

K, /K	0.10	M1		M2		M3	
$n_b/n_c$	\$6/\$c	No.	NMSE	No.	NMSE	No.	NMSE
		$\operatorname{coef}$	(dB)	coef	(dB)	$\operatorname{coef}$	(dB)
3	0	22	-34.05	22	-34.56	26	-35.38
3	1	24	-34.32	24	-34.96	28	-35.92
3	2	26	-34.64	26	-35.05	30	-36.00
3	3	28	-34.74	28	-35.14	32	-36.07
5	0	23	-34.05	24	-35.25	28	-36.27
5	1	26	-34.72	28	-35.99	32	-37.18
5	2	29	-35.10	32	-36.14	36	-37.35
5	3	32	-35.25	36	-36.27	40	-37.48
7	0	24	-34.05	26	-35.38	30	-36.42
7	1	28	-34.82	32	-36.31	36	-37.35
7	2	32	35.26	38	-36.53	42	-37.61
7	3	36	-35.43	44	-36.66	48	-37.80
9	0	25	-34.05	28	-35.46	32	-36.50
9	1	30	-34.86	36	-36.38	40	-37.43
9	2	35	-35.36	44	-36.61	48	-37.73
9	3	40	-35.58	52	-36.74	56	-37.94

 Table 1. NMSE comparison of different models.



Figure 5. EPSD plots for the single carrier 16QAM signal test.



Figure 6. Comparison of the output spectra for the 4-carrier WCDMA signal test.

and number of coefficients, compared with the HME model and the GMP model, the new proposed Volterra-based model uses the least coefficients but achieves the highest accuracy in both time and frequency domains.

## 4.2. DPD Performance Assessment

The proposed model, as well as the HME and GMP models were applied to DPD. The model dimensions were set to the values highlighted in Table 1 and Fig. 4. ACPR was considered to assess the DPD performance.

The measured ACPRs and number of coefficients for the 4-carrier WCDMA signal and the single carrier 16QAM signal are listed in Table 2 and Table 3 respectively. In comparison with the HME model, the proposed model shows significant ACPR improvements of  $2.90/1.34 \,\mathrm{dB}$  and  $2.61/3.54 \,\mathrm{dB}$  for the two test signals respectively, and a 20% reduction in the number of coefficients. The proposed model also outperforms the GMP model with ACPR improvements of  $2.26/0.42 \,\mathrm{dB}$  and  $1.38/0.82 \,\mathrm{dB}$  for the two test signals respectively, but with approximately 40% decrease in the number of coefficients. The measurement results in terms of ACPR demonstrate the superiority of the proposed model.

Figures 6 and 7 show the comparison of the output spectra for the 4-carrier WCDMA signal and the single band 16QAM signal, respectively. The figures prove that the proposed model achieves the best DPD performance once again.

DPD approaches	ACPR of upper	ACPR of lower	No. coef	
DI D'approaches	band (dBc)	band (dBc)		
DPD OFF	-22.53	-24.41		
DPD M1	-47.69	-48.68	40	
DPD M2	-48.33	-49.60	52	
DPD M3	-50.59	-50.02	32	

Table 2. Comparison of ACPRs for 4-carrier WCDMA signal.

Table 3.	Comparison	of ACPRs	for single	carrier 1	6QAM	signal.
----------	------------	----------	------------	-----------	------	---------

DPD approaches	ACPR of upper band (dBc)	ACPR of lower band (dBc)	No. coef
DPD OFF	-34.32	-36.61	
DPD M1	-46.49	-46.55	40
DPD M2	-47.72	-49.27	52
DPD M3	-49.10	-50.09	32



Figure 7. Comparison of the output spectra for the single carrier 16QAM signal test.

## 5. CONCLUSION

In this paper, a new accurate Volterra-based model is proposed for behavioral modeling and DPD of RF PAs. It extends the GMP model with specific cross terms, and these augmented terms significantly increase the model's performance. The model's performance in the behavioral modeling and DPD of a highly nonlinear Doherty PA driven by two signals (a 4-carrier WCDMA signal and a single carrier 16QAM signal) was assessed and compared to that of the HME and GMP models. In the behavioral modeling application, the calculated results in terms of NMSE, EPSD and number of coefficients indicate that the proposed model achieves the highest accuracy with the lowest computational complexity. In the DPD application, the measurement results also clearly demonstrate the superiority of the proposed model.

### ACKNOWLEDGMENT

This work was supported in part by Important National Science & Technology Specific Projects (No. 2010ZX03007-003-04), National Natural Science Foundation of China (No. 61001060), and the Fundamental Research Funds for the Central Universities (No. 2012RC0301).

### REFERENCES

1. Xu, G., T. Liu, Y. Ye, and T. Xu, "FPGA implementation of augmented Hammerstein predistorters for RF power amplifier linearization," *Proceedings* — 2009 3rd IEEE International Symposium on Microwave, Antenna, Propagation and EMC Technologies for Wireless Communications, 481–484, Beijing, China, Oct. 2009.

- El Maazouzi, L., A. Mediavilla, and P. Colantonio, "A contribution to linearity improvement of a highly efficient PA for WIMAX applications," *Progress In Electromagnetics Research*, Vol. 119, 59–84, 2011.
- Hashmi, M. S., Z. S. Rogojan, and F. M. Ghannouchi, "A flexible dual-inflection point RF predistortion linearizer for microwave power amplifiers," *Progress In Electromagnetics Research C*, Vol. 13, 1–18, 2010.
- Zhu, A., M. Wren, and T. J. Brazil, "An efficient Volterra-based behavioral model for wideband RF power amplifiers," 2003 IEEE MTT-S International Microwave Symposium Digest, Vol. 2, 787– 790, 2003.
- 5. Zhu, A. and T. J. Brazil, "Behavioral modeling of RF power amplifiers based on pruned Volterra series," *IEEE Microw. Wireless Compon. Lett.*, Vol. 14, No. 12, 563–565, Dec. 2004.
- Zhu, A., J. C. Pedro, and T. J. Brazil, "Dynamic deviation reduction-based Volterra behavioral modeling of RF power amplifiers," *IEEE Trans. Microw. Theory Tech.*, Vol. 54, No. 12, 4323–4332, Dec. 2006.
- Crespo-Cadenas, C., J. Reina-Tosinaand María, and J. Madero-Ayora, "Volterra behavioral model for wideband RF amplifiers," *IEEE Trans. Microw. Theory Tech.*, Vol. 55, No. 3, 449–457, Mar. 2007.
- 8. Carlos, C. C., R. T. Javier, and J. M. A. María, "A new approach to pruning Volterra models for power amplifiers," *IEEE Trans. Signal Process.*, Vol. 58, No. 4, 2113–2119, Apr. 2010.
- Ding, L., G. T. Zhou, D. R. Morgan, Z. Ma, J. S. Kenney, J. Kim, and C. R. Giardina, "A robust digital baseband predistorter constructed using memory polynomials," *IEEE Trans. Commun.*, Vol. 52, No. 1, 159–165, Jan. 2004.
- Hammi, O., M. Younes, and A. Kwan, "Performance-driven dimension estimation of memory polynomial behavioral models for wireless transmitters and power amplifiers," *Progress In Electromagnetics Research C*, Vol. 12, 173–189, 2010.
- Hammi, O., F. M. Ghannouchi, and B. Vassilakis, "A compact envelope-memory polynomial for RF transmitters modeling with application to baseband and RF-digital predistortion," *IEEE Microw. Wireless Compon. Lett.*, Vol. 18, No. 5, 359–361, May 2008.

- 12. Hammi, O., M. Younes, and F. M. Ghannouchi, "Metrics and methods for benchmarking of RF transmitter behavioral models with application to the development of a hybrid memory polynomial model," *IEEE Trans. Broadcast.*, Vol. 56, No. 3, 350– 357, Sep. 2010.
- Morgan, D. R., Z. Ma, J. Kim, M. G. Zierdt, and J. Pastalan, "A generalized memory polynomial model for digital predistortion of RF power amplifiers," *IEEE Trans. Signal Process.*, Vol. 54, No. 10, 3852–3860, Oct. 2006.
- Landin, P., M. Isaksson, and P. Handel, "Comparison of evaluation criteria for power amplifier behavioral modeling," *Proc. IEEE MTT-S Int. Microw. Symp.*, 1441–1444, Atlanta, GA, Jun. 2008.
- Isaksson, M., D. Wisell, and D. Rönnow, "A comparative analysis of behavioral models for RF power amplifiers," *IEEE Trans. Microw. Theory Tech.*, Vol. 54, No. 1, 348–359. Jan. 2006.
- Guan, L. and A. Zhu, "Simplified dynamic deviation reductionbased Volterra model for Doherty power amplifiers," *Integrated Nonlinear Microwave and Millimetre-wave Circuits (INMMIC-*2011), 1–4, Vienna, Austria, Apr. 2011.
- Younes, M. and O. Hammi, "An accurate complexity-reduced "PLUME" model for behavioral modeling and digital predistortion of RF power amplifiers," *IEEE Trans. Ind. Electron.*, Vol. 58, No. 4, 1397–1405, Apr. 2011.