# NOVEL KU BAND FAN BEAM REFLECTOR BACK ARRAY ANTENNA

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Abstract—In this paper, a Ku band fan beam reflector back array antenna is introduced. This is made up of two main parts that are planar array and main reflector. The proposed antenna has dimensions of  $103.3 \times 27.5 \times 12 \text{ mm}^3$  including the reflector. This antenna with high gain for incorporating in Ku band radars at 13.4–14 GHz is described. The fan beam radiation patterns with monopolar characteristics i.e., the cross-polarization is at least 10 dB lower than the co-polarization and are obtained in the frequency band of interest. The maximum gain for proposed antenna is 16.6 dBi at 13.75 GHz and the peak gain generally >16 dBi throughout the frequency band of interest.

# 1. INTRODUCTION

In recent years, the demand for wireless communication services has advanced from fixed narrow bands to radar and mobile broadband services. The capability of a mobile antenna system should provide wireless internet services, wireless LAN and multimedia services, as well as high quality broadcasting services simultaneously on moving vehicles via Ku-band geo-stationary satellites. Reflector antennas with mechanical beam steering occupy an important place in the area of mobile and radar communication systems [1-10]. They make possible high gain and an admissible side lobe level at minimum cost and light weight. Recently, a shaped array antenna with an elongated main reflector and a sub-radiator was utilized in several projects (for example in [1-3]). It has a low profile design along with a high gain fan beam. Also, due to an almost reflector aperture, a feed with axial symmetry operating at both a linear and a circular polarization and providing a low cross-polarization can be used. At the same time, the aforementioned antennas have a sub-array located in the central part of the main reflector aperture that creates a blockage effect.

In this paper, a Ku band fan beam reflector back array antenna is introduced. This is made up of two main parts that are planar array and main reflector. The proposed antenna has dimensions of  $103.3 \times 27.5 \times 12 \text{ mm}^3$  including the reflector. This antenna has high gain suitable for incorporating Ku band radars in 13.4–14 GHz (This is one of the two frequency band that International Telecommunications Union (ITU) allocated to radars in Ku band [11]) is described. In advance, results including return losses, radiation patterns and gain variations are presented and discussed.



Figure 1. Geometrical parameters of antenna with band notch characteristics.

### 2. ANTENNA DESIGN

The antenna geometry is shown in Figs. 1(a)-(d). This antenna is made up of two main parts that are planar array and main reflector. The array part of this antenna is constructed on Rogers TMM 10i substrate with thickness  $\sim 508 \,\mathrm{mm}$  (20 mil), relative dielectric constant  $\varepsilon_r$  of 9.8 and  $\tan \delta = 0.0020$  which has a dimension of  $9.5 \times 100 \text{ mm}^2 (W_{sub} \times L_{sub})$ . This is array of conventional hexagonal planar monopole antenna. Also, the feedline length and  $L_{gnd}$  are equal to  $L_{sub}$ . The width of transmission line,  $W_f = 0.48 \,\mathrm{mm}$  has been designed for approximately 50  $\Omega$  characteristic impedance and  $W_f$  has been calculated from (1) and (2) [12] for  $\varepsilon_r = 9.8$ , h = 0.508 mm and  $Z_0 = 50$  ohm. The remaining parameters of planar array are:  $W_2 = 4.01 \text{ mm}, W_{gnd} = 1.28 \text{ mm}, d_1 = 3.71 \text{ mm}, d_2 = 9.275 \text{ mm}$  and  $d_3 = 0.76 \,\mathrm{mm}$ . The reflector part is made from aluminum conductor with thickness  $t_r = 1.65 \,\mathrm{mm}$ . The ground of array is connected perpendicularly to reflector part (Fig. 2) and this means the reflector isn't parasitic element. The remaining parameters of planar array are:  $L_r = 101.65 \text{ mm}, W_1 = 17.55 \text{ mm}, h_1 = 12 \text{ mm} \text{ and } W_r = 15.67 \text{ mm},$  $C_1 = 9.87 \,\mathrm{mm}$  and  $\varphi_1 = 150 \,\mathrm{deg}$ .

$$\varepsilon_{eff} = \frac{\varepsilon_r + 1}{2} + \frac{\varepsilon_r - 1}{2} \frac{1}{\sqrt{1 + 12\frac{h}{w}}} \tag{1}$$

$$Z_0 = \frac{120\pi}{\sqrt{\varepsilon_{eff}} \left[\frac{w}{h} + 1.393 + 0.667 \ln\left(\frac{w}{h} + 1.444\right)\right]} \quad \text{for} \quad \frac{w}{h} \ge 1 \ (2)$$



Figure 2. The ground of array is connected perpendicularly to reflector to reflector part.

### 3. RESULTS

The comparison between magnitude of s-parameters simulation results with Ansoft HFSSv.10 [13] and CST MICROWAVE STUDIO [14] for proposed antenna is shown in Fig. 3. Plot shows the good match between two simulation results with different commercial software for proposed antenna. Start frequency for Ansoft HFSS results is 13.25 GHz while for CST MICROWAVE results is 12.85 GHz in measurements. Both results show good impedance match ref to VSWR < 2 throughout the 13.4–14 GHz (ITU Radar Ku Band Nomenclature) passband.



**Figure 3.** Magnitude of  $S_{11}$  for proposed antenna in dB.



Figure 4. The deviation of antenna from Y-axis.



Figure 5. Radiation patterns simulated in  $f = 13.4 \,\text{GHz}$ , top is  $\varphi = 90^{\circ}$  cut and bottom is  $\varphi = 0^{\circ}$  cut.

The radiation pattern is achieved by Ansoft HFSS and antenna had 12 deg deviations from Y-axis (Fig. 4). The plots correspond to operating bands of 13.4, 13.7 and 14 GHz are shown in Figs. 5-7 respectively.

The top row of each figure shows the  $\varphi = 90^{\circ}$  cut radiation while the bottom row shows the  $\varphi = 0^{\circ}$  cut radiation patterns. The radiation plots display very good monopolar mode radiation and at least, the cross-polarization is 10 dB lower than the co-polarization in all frequency. Table 1 shows main electrical performances of the

Frequency band	$3\mathrm{dB}$ Beam width	Side-lobe Level	Cross polarization
$13.4\mathrm{GHz}$	$13^{\circ} \times 57^{\circ}$	$10.06\mathrm{dBc}$	$10\mathrm{dBc}$
$13.7\mathrm{GHz}$	$11.25^{\circ} \times 49^{\circ}$	$10.55\mathrm{dBc}$	$18.5\mathrm{dBc}$
$14.0\mathrm{GHz}$	$10.2^{\circ} \times 40^{\circ}$	9.9 dBc	$17.26\mathrm{dBc}$

 Table 1. Main electrical performances of the radiation patterns.



Figure 6. Radiation patterns simulated in  $f = 13.7 \,\text{GHz}$ , top is  $\varphi = 90^{\circ}$  cut and bottom is  $\varphi = 0^{\circ}$  cut.



Figure 7. Radiation patterns simulated in  $f = 14.0 \,\text{GHz}$ , top is  $\varphi = 90^{\circ}$  cut and bottom is  $\varphi = 0^{\circ}$  cut.



Figure 8. Peak gain of proposed antenna in (dBi).

radiation patterns results.

The antenna peak gain (dBi) is depicted in Fig. 8. It reveals that the peak gain is very stable over the frequency band of interest and in both simulations results, the gain is about 16 dBi.

### 4. CONCLUSION

Fan beam antenna is made up of two main parts that are sub array and main reflector is introduced. The proposed antenna has dimensions of  $103.3 \times 27.5 \times 12 \text{ mm}^3$  including the reflector. This antenna has high gain suitable for incorporating Ku band radars in 13.4-14 GHz is described. The fan beam radiation patterns with monopolar characteristics are obtained over the frequency band of interest. The maximum gain for proposed antenna is in 13.75 GHzand this was equal to 16.6 dBi. These results shown that the sub-array is located in the central part of the main aperture can improve the radiation performance of antenna very well.

Since the proposed antenna technology permits the provision of diverse radar applications inculduding low profile portable radar systems.

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