Design and Measurement of Triple H-Slotted DGS Printed Antenna with Machine Learning

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Abstract—This paper presents the design and measurements of a dual-band Triple H-Defected Ground Structure (Triple H-DGS) antenna. DGS has proven to be successful in the design of multiband antennas; however because of the lack of a standard approach, the determination of the exact position of the Triple H-DGS requires rigorous and lengthy numerical computations. The aim of the current work is to present a state-of-the-art innovative, efficient, and accurate solution based on Machine Learning (ML) techniques. The design is based on Substrate Integrated Waveguide (SIW) technology which provides low cost, small size, and convenient integration with planar circuits. The antenna is fabricated on a Roger 5880 substrate with a thickness of 1.6 mm, relative dielectric constant of 2.2, and tangent loss of 0.0009. The proposed antenna was developed using a hybrid solution based on CST Microwave Studio assisted by ML, and the fabricated prototype was measured using both ROHDE & SCHWARZ ZVB20 network analyser and an anechoic chamber setting. The measurement results show good agreement with the simulation. The antenna demonstrates a dual-band performance at centre frequencies of 12.67 GHz and 14.56 GHz, for which the respective antenna gains are 7.03 dBi and 7.38 dBi, and antenna directivities of 7.77 dB and 8.13 dB, respectively. The antenna total efficiencies are 95.25% and 95.60%, at the corresponding centre frequencies. The developed ML based technique shows good accuracies of about 98% in the determination of the DGS position and saves more than 99% of the computational time. The developed antenna is compact, simple in structure, and can be used for different applications in the Ku band.

1. INTRODUCTION

The advancements in the microstrip antenna design technologies and techniques have been the key success factors in developing new promising wireless applications [1, 2], where size and ease of installation are vital considerations. However, antenna bandwidth and efficiency have deteriorated in many of the newly proposed antenna designs [3–6]. Several methods have been implemented to modify the antenna design in a way that alleviates such drawbacks [7]. This is achieved by adopting different feeding techniques, including microstrip line, coaxial probe, aperture coupling, and proximity [8].

Patch antenna designs can be altered in a way that makes them appropriate for multi-band wireless communications including multi-layer rectangular patch antenna array [9–12], a low-profile dual-band circular polarized antenna for a nanosatellite communication system [13], and multi-layered based on metasurface dual circularly polarized (CP) patch antenna [14] achieving a broadband operating frequency band. The main drawbacks of the aforementioned designs are the difficulty of their fabrication due to the air gap between layers and some alignment issues. Furthermore, using the coaxial feeding technique makes the design unsuitable for integrated circuit configuration and incompatible for the

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use as a planar antenna. Alternatively, the use of Defected Ground Structures (DGSs) has proven to be a successful method for obtaining multiband resonances through current disturbances created on the surface of the structure. This technique has been used in the filter design and in antennas development [15–23].

This paper presents a novel technique to address the lack of a standard approach for determining the exact position of a slotted Triple H-DGS in regard to particular resonance frequencies by providing an innovative, efficient, and accurate solution based on Machine Learning. The current paper is structured as follows. The first part presents the proposed antenna design. The following sections concentrate on the optimization of the position of a Triple-HDGS to achieve the required resonance frequencies of the antenna and with the use of our proposed machine learning based approach. Besides, the fabrication and measurement of the Triple-HDGS antenna for the aim to validate our proposed approach are conducted. The fabricated antenna is then measured on ROHDE & SCHWARZ ZVB20 network analyser for the return loss and a chamber setting for the radiation parameters.

2. ANTENNA DESIGN

Figures 1 and 2 present the SIW geometry, the Triple-HDGS unit cell which is found to be optimum with respect to the required resonance bands based on our previous study in [16], and the overall proposed antenna structure, respectively. Table 1 depicts all dimensions. Figure 3 shows the fabricated antenna. The developed antenna is based on Roger/Duroid5880 (relative permittivity and loss tangent of 2.2 and 0.0009, respectively) and a thickness of $H_{sub} = 1.6$ mm for the substrate material.



Figure 1. The geometry of H-DGS unit cell.

 Table 1. Design parameters of the proposed antenna.

Variables	Α	В	AA	BB	Af	G2	G3	Р	d	L1	Af
Value (mm)	45.5	37	19	23	31	7	8.6	0.75	0.4	3	31
Variables	Bf	As	Wg	Wf	G1	L1	L2	L3	L 4	G1	Hsub
Value (mm)	5	1.6	17	1.75	4.5	3	1.5	1.5	0.5	4.5	1.6

3. MACHINE LEARNING AND EXPERIMENTAL RESULTS

With the aim of automating the design of a dual-band antenna using DGS based technology, Artificial Neural Network (ANN) modelling is used. The motivation behind to use ANN for the prediction of the optimal position of Triple H-DGS is the lack of a standard approach that can be used to determine the exact position of any DGS geometry in regard to a particular resonance frequency [24, 25]. The position of the Triple H-slotted DGS controls the resonance frequencies in terms of dual or a single resonance.



Figure 2. Schematic diagram of the proposed antenna. (a) Top view. (b) Bottom view.



Figure 3. Unit cell of the H shaped DGS. (a) Top view. (b) Bottom view.

The ANN based model is developed using a MATLAB code to produce resonance frequencies and return losses (S_{11}) as output parameters with the consideration of the position values of the Triple H-slotted DGS as input (X pos & Y pos). These values should be within the patch ground plane limits. Table 2 lists the results obtained from both the CST and ANN simulations in terms of X, Y positions, resonance frequencies, and return losses (S_{11}) . Figure 5 depicts that an optimal return loss is obtained when the position of the DGS is at the centre of the ground plane.

In order to validate our developed ANN model, the mean square error (MSE) using Equation (1) [26] is calculated and reported in Table 3.

$$RMSE = \sqrt{\frac{1}{n}} \sum_{i=1}^{n} (t_i - \alpha_i)^2$$
(1)

where n is the total number of samples, and t_i and α_i represent the target and output data, respectively.

		In		Ta	rgets	Outputs		
		mput		(Simulate	$\mathbf{ed} \mathbf{by} \mathbf{CST}$	(Estimated by ANN)		
		X Position	Y Position	Freq	S_{11}	Freq	S_{11}	
				(GHz)	(dB)	(GHz)	(dB)	
				13	12	12.98	11.97	
	01	-2	1	14.1	15.66	14	15.59	
Training	02	-2	-2	13.7	20.6	13.25	20.4	
Data								
Data								
	74	-1	1	14.36	25.2	14.38	24.98	
	75	-1	0	11.34	28.5	11.32	28.47	
				12.7	12.1	12.68	11.98	
	76	0	1	14.4	11.5	14.38	11.48	
Validation Data	77	1	0	12.5	22	12.37	21.9	
	89	-1	-2	14.38	24.08	14.35	24.06	
	90	1	1	12.5	45.6	12.47	45.72	
Testing Data				12.7	14.8	12.68	14.77	
	91	0	-1	14.4	11.6	14.37	11.57	
				14.56	14.52	14.53	14.5	
	92	0	0	12.6	18.1	12.58	17.89	
	99	1	-2	12.48	27.3	12.52	27	
	100	1	-1	12.5	28	12.47	27.89	

Table 2. A comparison between the obtained ANN and simulated CST results.

Table 3. Mean Square Error (MSE) for our developed ANN model.

Design Parameters	Mean Square Error (MSE)						
Design 1 arameters	Freq 01 (GHz)	$S_{11}~(\mathrm{dB})$	Freq 02 (GHz)	$S_{11}~(\mathrm{dB})$			
Optimal X & Y Position	0.0662	0.0287	0.0099	0.0208			

The testing error is represented as a function of Regression R-value (R-value close to 1 means that the ANN model is well trained, tested, and validated) [27] as shown in Figure 4, respectively. From the calculated MSE, extracted R-value graphs, we can notice that our developed ANN model has a good performance. Lastly, there is a save of about 99% of the computational time while maintaining a prediction error below 2%.

As an experimental validation, Figure 6 compares the reflection coefficient values obtained from simulation with those obtained from measurement. It is found that the proposed antenna has two resonance frequencies at 12.58 GHz and 14.64 GHz frequencies with bandwidths of 100 MHz and 230 MHz at the two frequencies, respectively. From Figure 7, it can be noticed that the gains at the two frequencies 12.67 and 14.56 are 7.03 dB and 7.38 dBi. The proposed antenna achieved radiation efficiencies of about 95.25% and 95.60% at 12.67 GHz and 14.56 GHz, respectively as displayed in Figure 7. Lastly, the radiation patterns at H and E planes are sketched in Figure 8. One notices that the maximum radiation is observed to be at 0° degrees. One can also notice the slight differences between the simulated and measured results, which are introduced by the SMA connectors and the environment in which the measurements are conducted.





Figure 4. Regression R-values.

Figure 5. Simulated reflection coefficients for different X pos & Y pos values.





Figure 6. Simulated and measured results. (a) Reflection coefficients. (b) Setup of network analyser and anechoic chamber.

The surface current distributions at 12.67 GHz and 14.56 are shown in Figures 9(a) and (b). It can be noticed that the surface currents are mainly distributed around the Triple H-DGS slotted in the ground layer and the vias placed in the top and bottom. Thus, the dual-band response is mainly caused by the Triple H-DGS.



Figure 7. Simulated and measured realized gain & antenna efficiency.



Figure 8. Simulated radiation patterns (a) at 12.67 GHz, (d) at 14.56 GHz.



Figure 9. Surface current distribution (a) at 12.67 GHz, (b) at 14.56 GHz.

A quantitative comparison is made with other similar reported studies in the literature [24–28] and listed in Table 4. Our developed antenna with ML has a higher realized gain over [24–27] yet having a lower antenna dimension. However, whereas the work presented in [28] shows a slightly higher gain, our suggested antenna has a superior lower dimension.

References	Frequency Bandwidth (CHz)	Gain (dB)	Radiation Efficiency	Dimension	
	Danuwiutii (G112)	(uD)	Enciency		
Bof [28]	2.7	1.1	NΛ	10 7 × 31 2	
	11	6		10.1 / 01.2	
D of [90]	16	6.9	NA	8×8	
nei. [29]	30	5.9	INA		
D .f [20]	3.5	10.2	NI A	95 imes 65	
nei. [30]	5.8	8.94	INA		
D.f. [91]	3.5	1.07	NT A	15 imes25	
nei. [51]	5.2	2.96	INA		
Ref. [32]	Case 01: 4.75 5.05	6 92		15 × 95	
(Reconfigurable)	Case 02: 5.11 5.18	0.02	INA	10 X 20	
Our Antonno	12.67	7.03	95.25	10 × 22	
Our Antenna	14.56	7.38	95.60	19 X 23	

Table 4. Comparison with previous semilar antennas.

4. CONCLUSION

The current study presents a novel machine learning based technique to accelerate the development of DGS-based patch antennas. The motivation behind this work is the lack of a standard approach for determining the exact position of a DGS in regard to a particular resonance frequency. The current approach considers the development of a patch antenna based on SIW Triple H-slotted DGS geometry. The proposed design is fabricated on a Roger 5880 substrate with a thickness of 1.6 mm, relative dielectric constant of 2.2, and tangent loss of 0.0009. The obtained results show a dual-band behaviour at 12.67 GHz and 14.56 GHz frequencies with gains of 7.03 dBi and 7.38 dBi, respectively. The antenna's total efficiencies are 95.25% and 95.60% at the two frequencies. The ML-based approach predicts the position of the DGS with the accuracy of about 98%.

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